

Prospective LCA modelling

How to deal with uncertainties ?

Part I : A new approach based on GSA

Part II : The Graphene Case study

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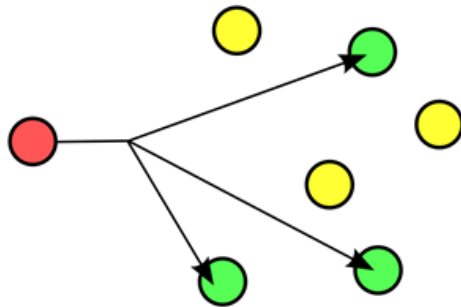
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Part I

Global sensitivity analysis in LCA of emerging technologies:

Accounting for inputs' variability



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LCA of emerging technologies: addressing high uncertainty on inputs' variability when performing global sensitivity analysis; Science of the Total Environment, 578 (2017) 268-280

Emerging technologies

- Wide data gap
- No pilot/large-scale data?
- Incomplete technology development
- Unknown future applications
- Data quality concerns



Increased level of
UNCERTAINTY



How to deal with
uncertainty in LCA of
emerging technologies?

EGS: an emerging technology to exploit geothermal resources where water, heat or rock permeability are not sufficient for a conventional geothermal system

- Deep wells: 2.5 – 5 km → Drilling
- Reservoir stimulation (enhancement) → Fracturing the rock (e.g. by water pumping)
- For binary systems → Organic Rankine cycle
- Ground-water use



Environmental impacts ?

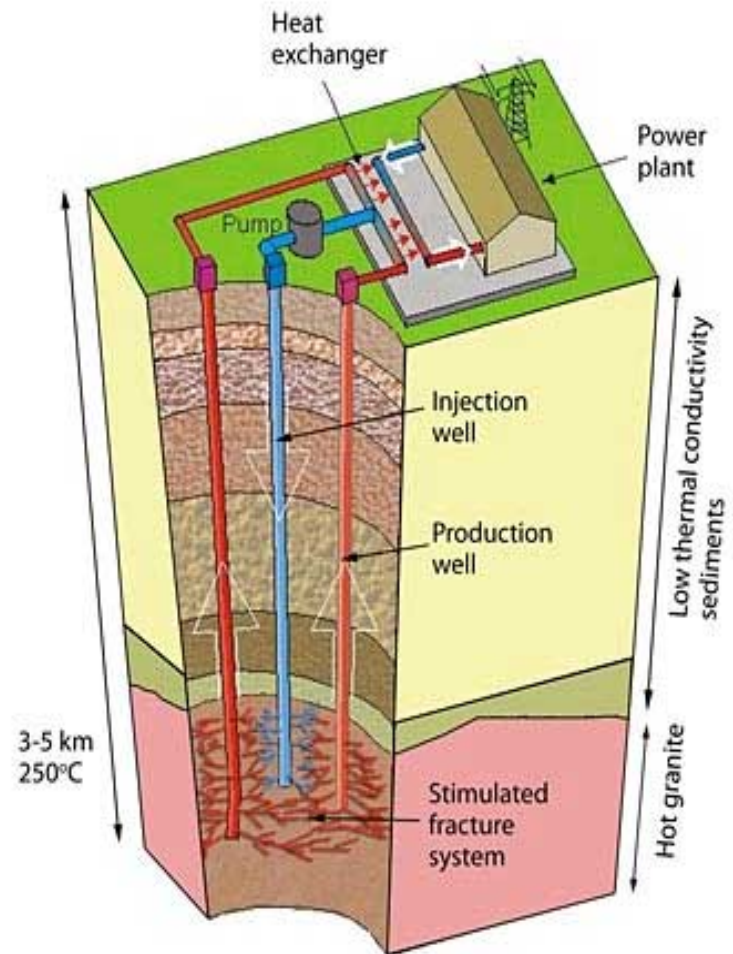
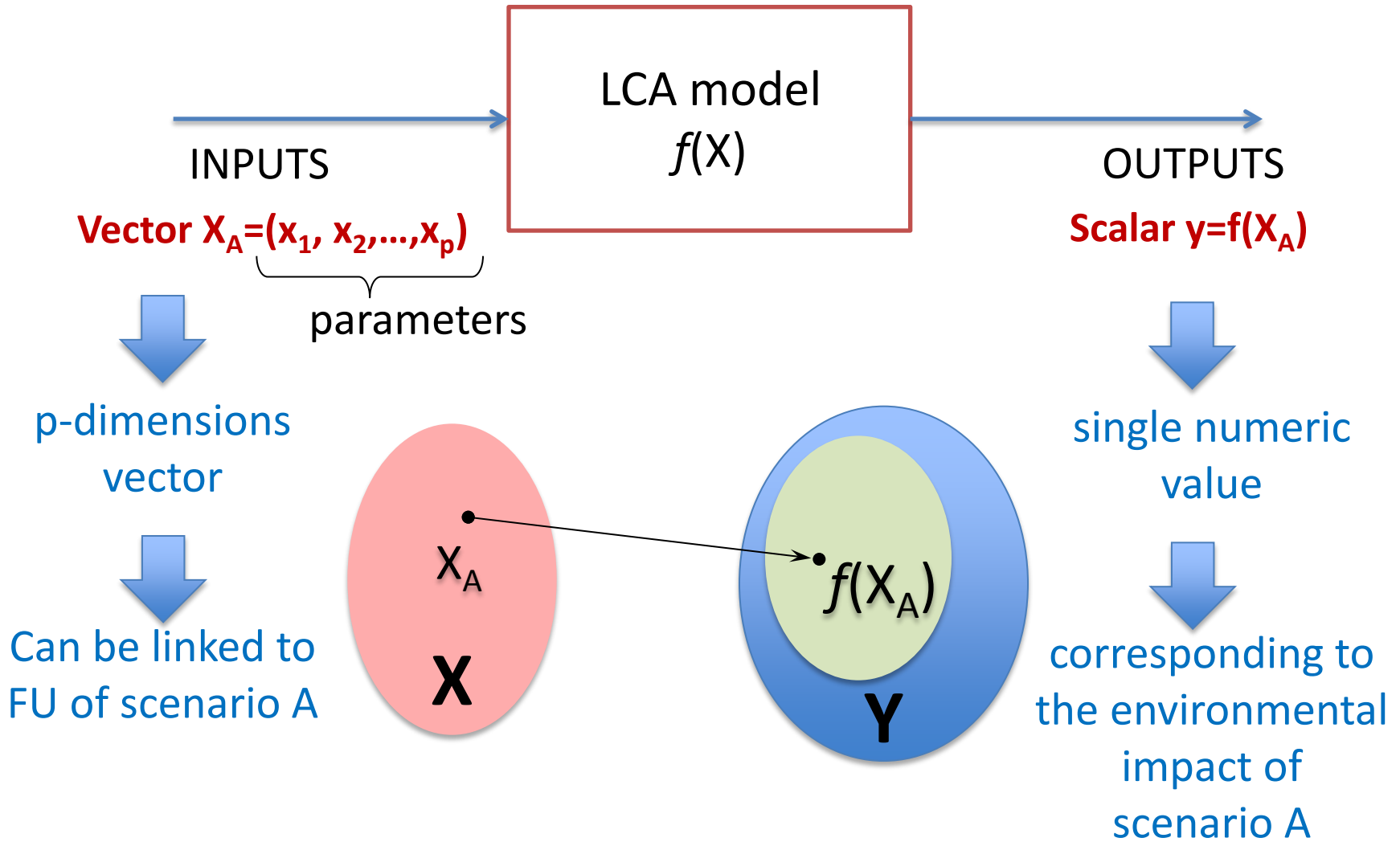
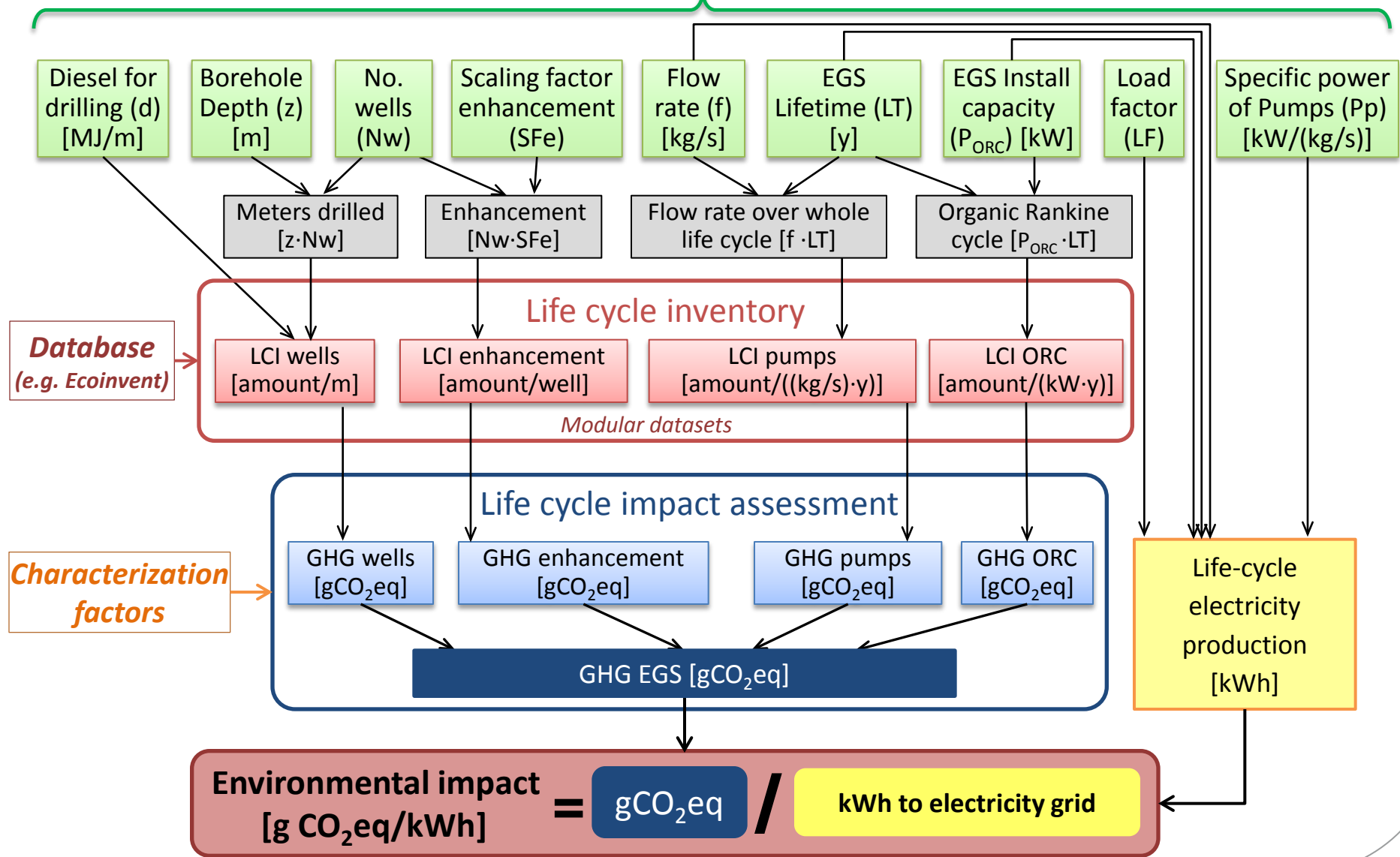


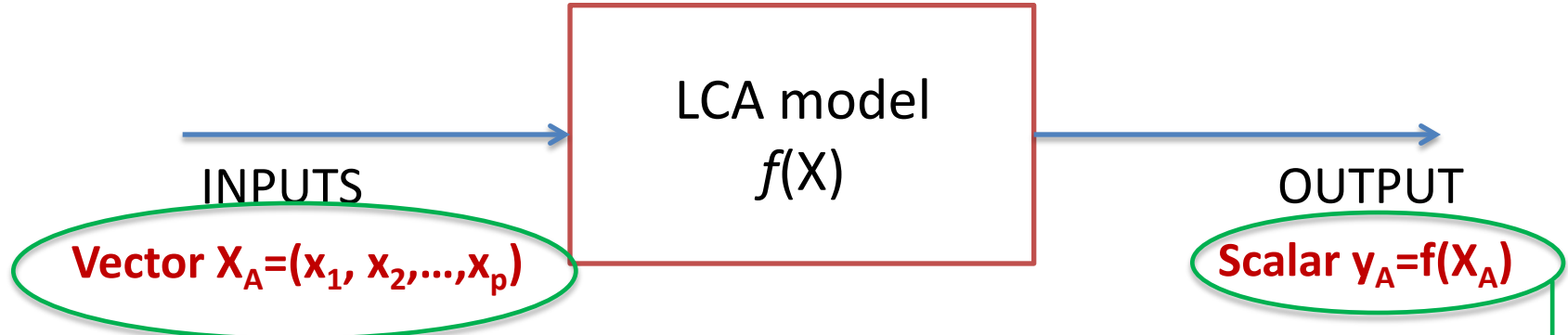
Image: geothermalworldwide, 2016



9 independent input parameters



Symbol	Parameters	Baseline scenario
z	Borehole depth	4000 m
Nw	Number of wells	3 wells
d	Fuel for drilling	5000 MJ/m
LT	Lifetime	30 y
f	Produced flow rate	62.5 kg/s
P _{ORC}	Installed capacity ORC	2375 kW
SFe	Enhancement scaling factor	5.25
LF	Load factor	0.90
P _p	Specific power of pumps	6.1 kW/(kg/s)



$$X_A = (z_A, Nw_A, d_A, LT_A, f_A, P_{ORC,A}, SFe_A, LF_A, P_{p,A})$$

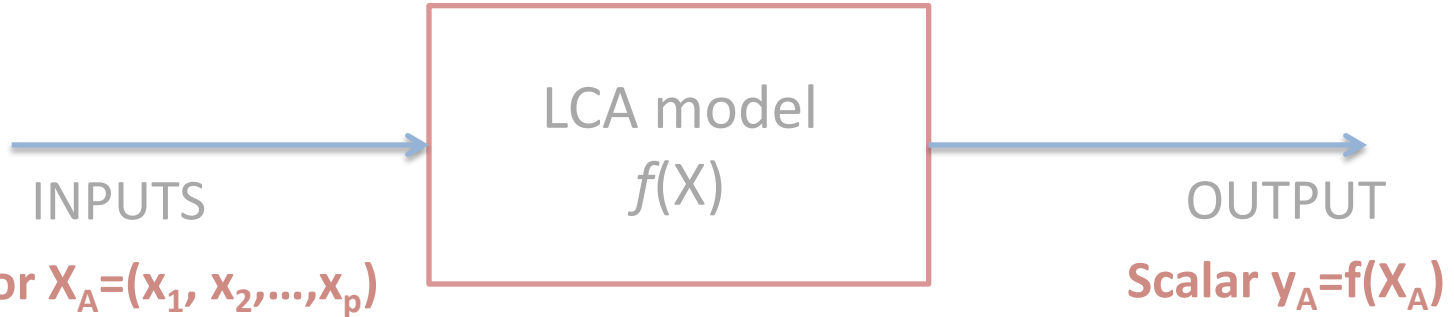
e.g. $X_A = (4000, 3, 5000, 30, 62.5, 2375, 5.25, 0.90, 6.1)$ →

$$y_A = 34.7 \text{ g CO}_2 \text{ eq/kWh}$$

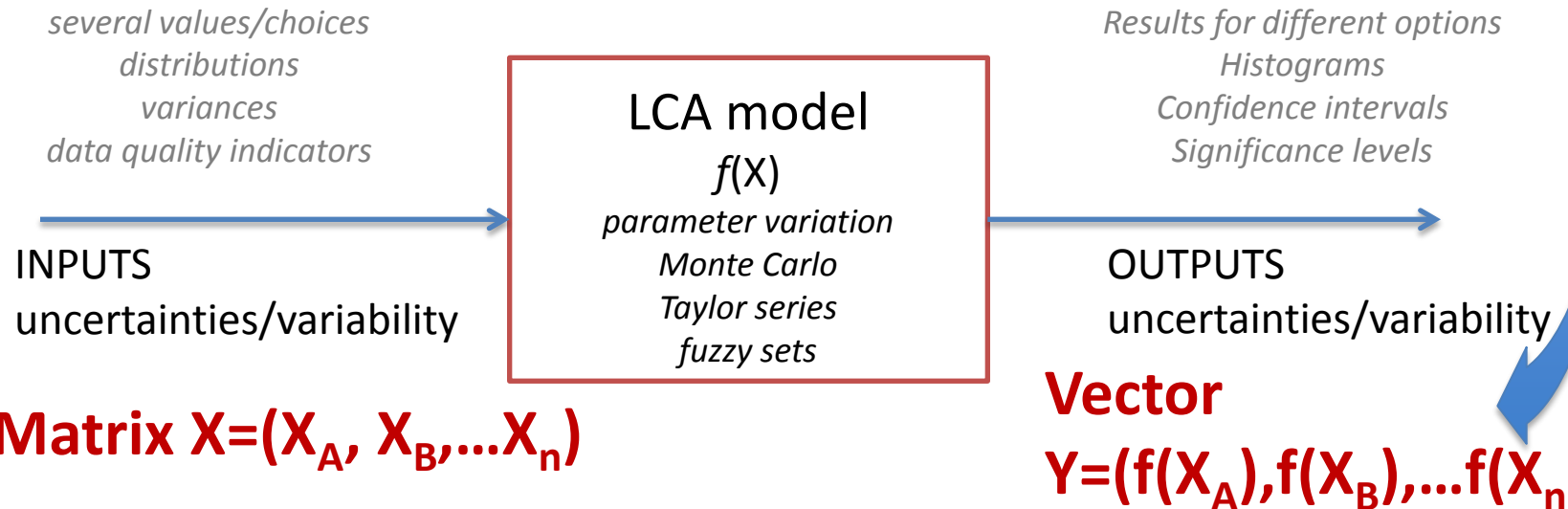
$$GHG_{EGS,A} \left[\frac{\text{g CO}_2 \text{ eq}}{\text{kWh}} \right] = \frac{z_A \cdot Nw_A \cdot (\alpha_1 + \alpha_2 \cdot d_A) + LT_A \cdot f_A \cdot \alpha_3 + P_{ORC,A} \cdot LT_A \cdot \alpha_4 + Nw_A \cdot Sfe_A \cdot \alpha_5}{LF_A \cdot LT_A \cdot (P_{ORC,A} - f_A \cdot P_{p,A}) \cdot 8760}$$

With $\alpha_1 = 498761.36 \text{ gCO}_2 \text{ eq/m}$; $\alpha_2 = 90.56 \text{ gCO}_2 \text{ eq/MJ}$; $\alpha_3 = 487363.03 \text{ gCO}_2 \text{ eq}\cdot\text{s}/(\text{kg}\cdot\text{y})$;
 $\alpha_4 = 50603.13 \text{ gCO}_2 \text{ eq}/(\text{kW}\cdot\text{y})$; $\alpha_5 = 25757089.05 \text{ gCO}_2 \text{ eq}$

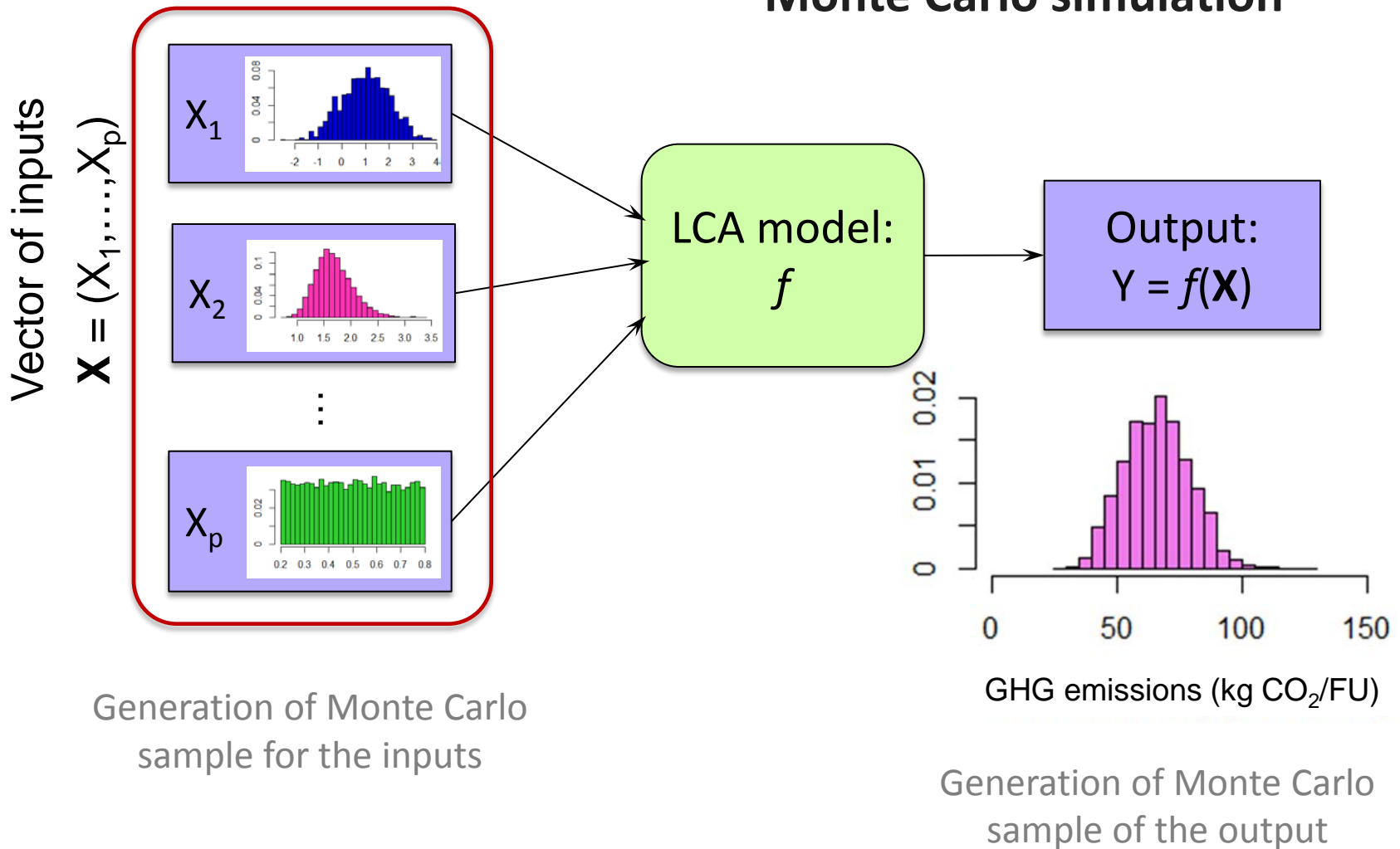
Symbol	Parameters	Baseline scenario	Value range
z	Borehole depth	4000 m	2000 – 6000 m
N _w	Number of wells	3 wells	2 – 3 wells
d	Fuel for drilling	5000 MJ/m	3000 – 7000 MJ/m
LT	Lifetime	30 y	20 – 40 y
f	Produced flow rate	62.5 kg/s	25 – 100 kg/s
P _{ORC}	Installed capacity ORC	2375 kW	1250 – 3500 kW
S _{Fe}	Enhancement scaling factor	5.25	0.5 – 10
LF	Load factor	0.90	0.85 – 0.95
P _p	Specific power of pumps	6.1 kW/(kg/s)	3.6 – 8.6 kW/(kg/s)

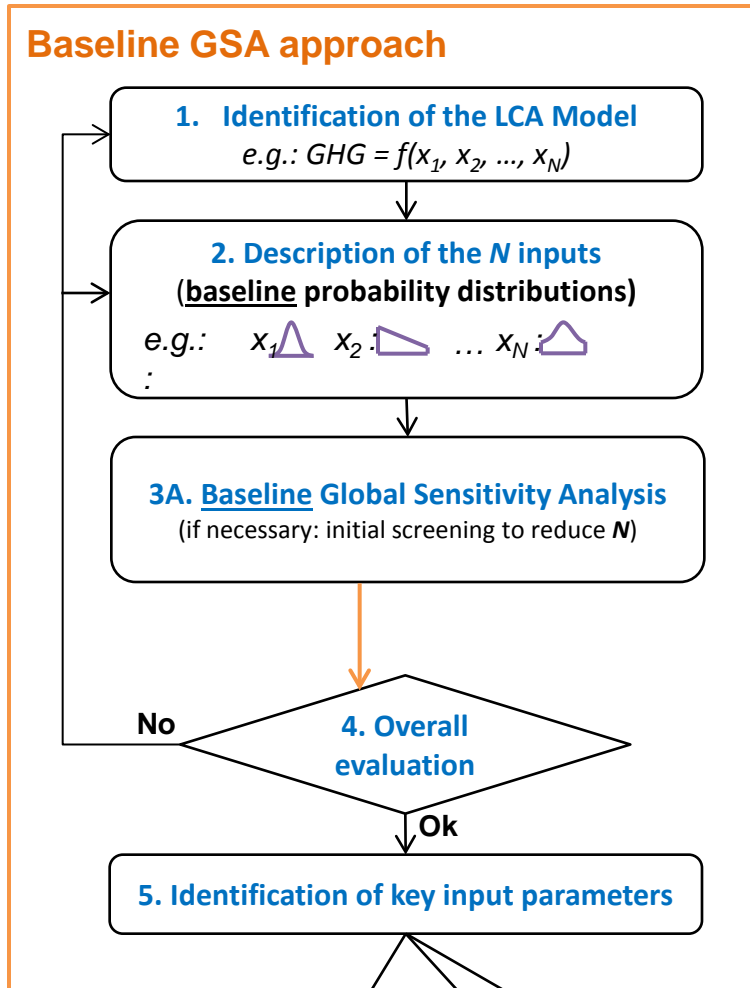


B) Modelling framework for LCA when dealing with uncertainties



Generation of scenarios by Monte Carlo simulation





$$GHG_{EGS,A} \left[\frac{g \text{ CO}_2eq}{kWh} \right] = \frac{z_A \cdot Nw_A \cdot (\alpha_1 + \alpha_2 \cdot d_A) + LT_A \cdot f_A \cdot \alpha_3 + P_{ORC,A} \cdot LT_A \cdot \alpha_4 + Nw_A \cdot Sfe_A \cdot \alpha_5}{LF_A \cdot LT_A \cdot (P_{ORC,A} - f_A \cdot P_{p,A}) \cdot 8760}$$

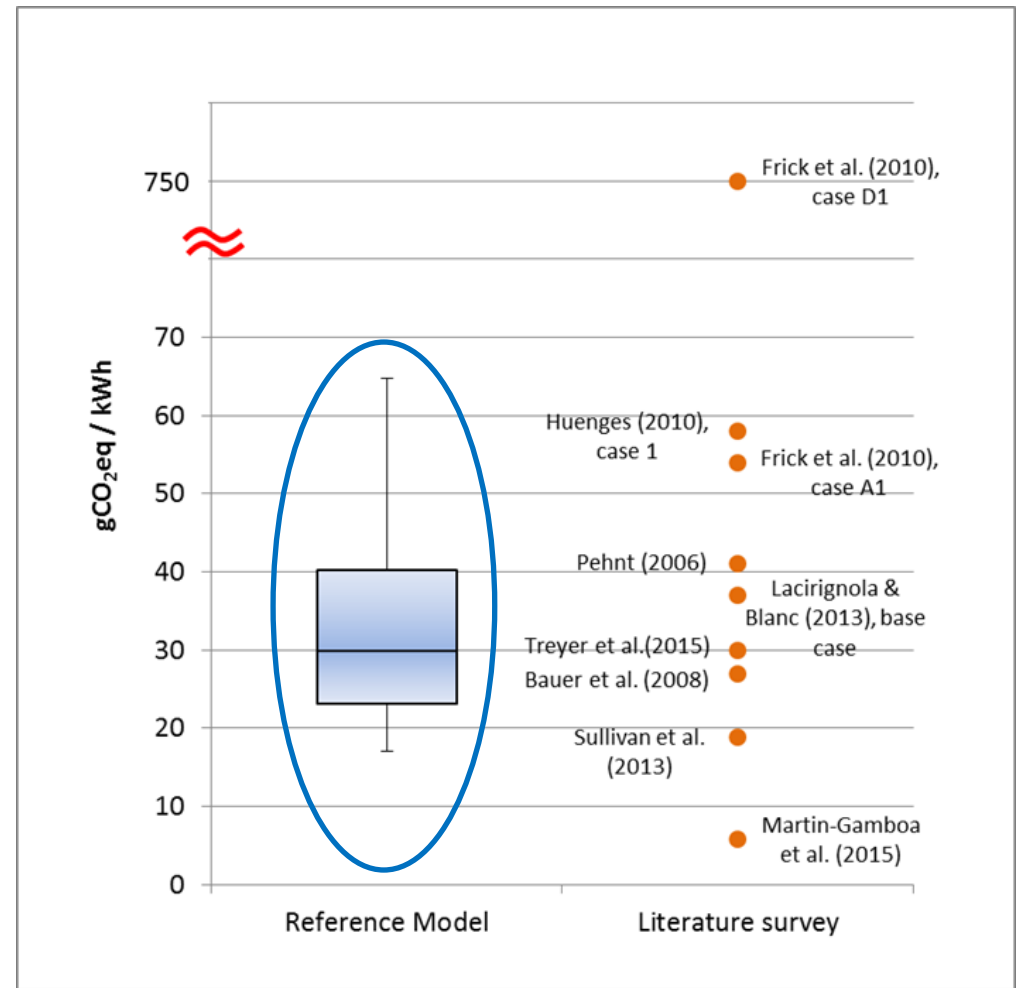
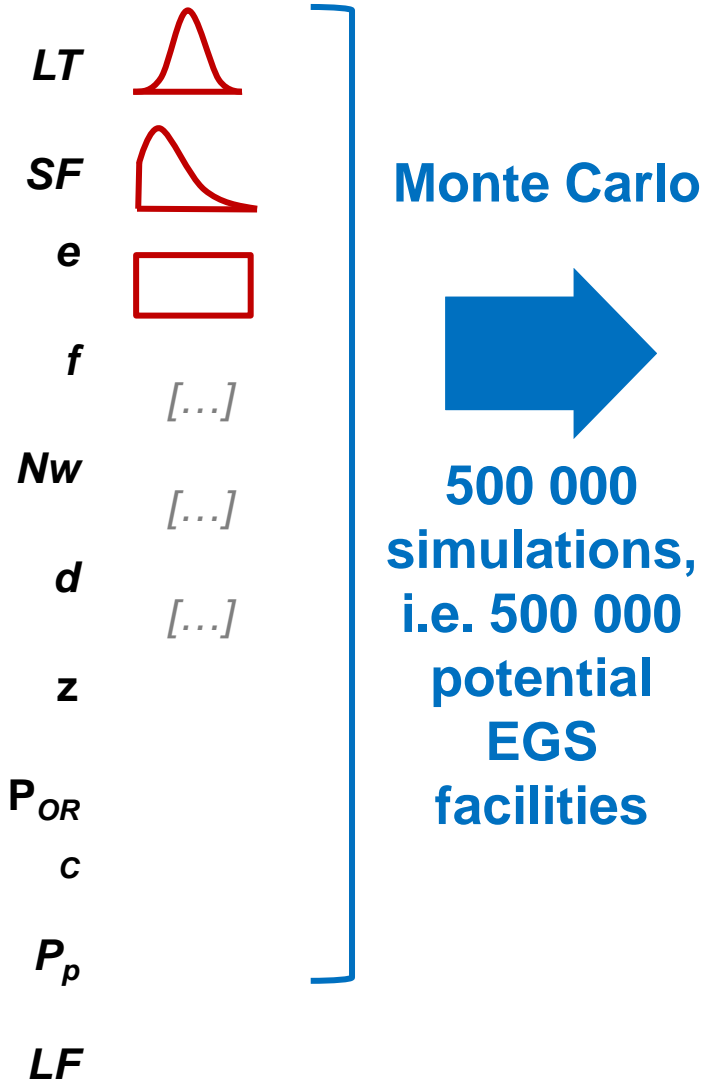
Applications:

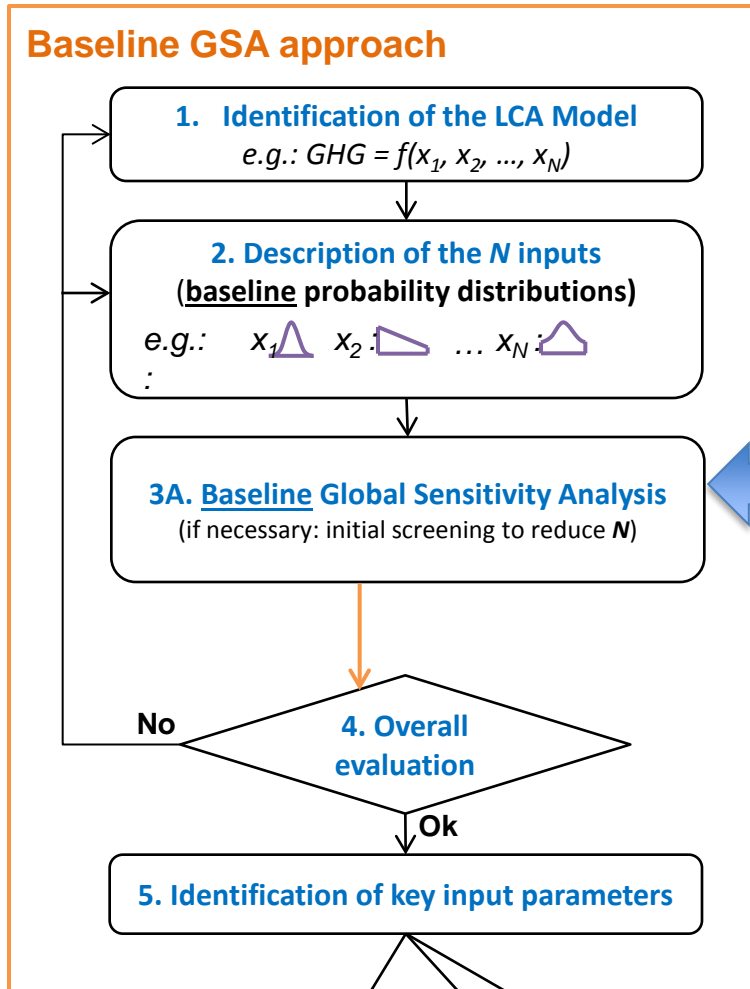
Simplified model

Other applications

(Cucurachi et al. 2016; Lacirignola et al. 2017)

Symbol	Parameters	Value range	Probability distribution
z	Borehole depth	2000 – 6000 m	Uniform
N_w	Number of wells	2 – 3 wells	Uniform
d	Fuel for drilling	3000 – 7000 MJ/m	Uniform
LT	Lifetime	20 – 40 y	Normal distribution centered on $LT=30$ with $\sigma=3.25$
f	Produced flow rate	25 – 100 kg/s	Uniform
P_{ORC}	Installed capacity ORC	1250 – 3500 kW	2375 kW
S_{Fe}	Enhancement scaling factor	0.5 – 10	Lognormal distribution with $\sigma=1$, $\mu=0$ and peak on $S_{fe}=1$
LF	Load factor	0.85 – 0.95	Uniform
P_p	Specific power of pumps	3.6 – 8.6 kW/(kg/s)	Uniform





$$GHG_{EGS,A} \left[\frac{g \text{ CO}_2 \text{ eq}}{kWh} \right] = \frac{z_A \cdot NW_A \cdot (\alpha_1 + \alpha_2 \cdot d_A) + LT_A \cdot f_A \cdot \alpha_3 + P_{ORC,A} \cdot LT_A \cdot \alpha_4 + NW_A \cdot Sfe_A \cdot \alpha_5}{LF_A \cdot LT_A \cdot (P_{ORC,A} - f_A \cdot P_{p,A}) \cdot 8760}$$

Based on Sobol indices (variance decomposition method) to identify key parameters:

$$S_i = \frac{Var[E(Y|X_i)]}{Var(Y)} = \frac{V_i(Y)}{Var(Y)}$$

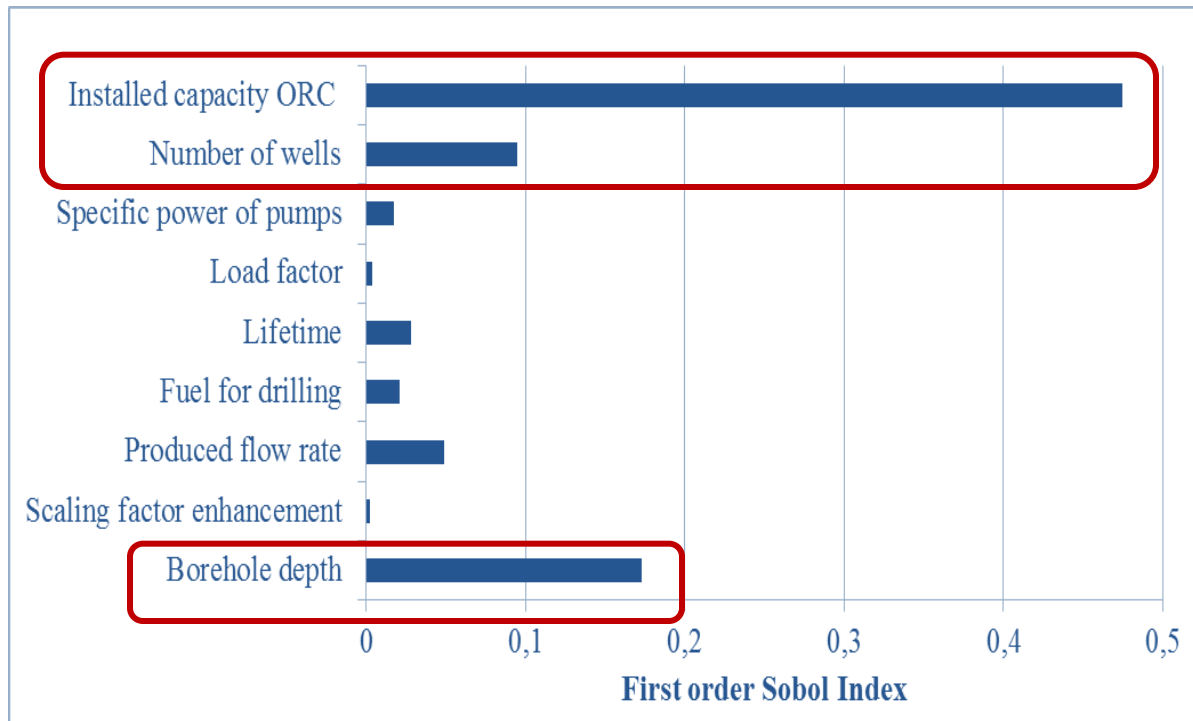
$$S_{ij} = \frac{V_{ij}(Y)}{Var(Y)} \quad S_{ijk} = \frac{V_{ijk}(Y)}{Var(Y)}$$

Applications:

Simplified model

Other applications

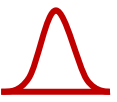
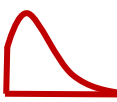

(Cucurachi et al. 2016; Lacirignola et al. 2017)



P_{ORC}, N_w, z



Key parameters
responsible for
75% of output
variation

- LT** 
- SF** 
- e** 
- f** [...]
- Nw** [...]
- d** [...]
- z**
- P_{OR}**
- c**
- P_p**
- LF**

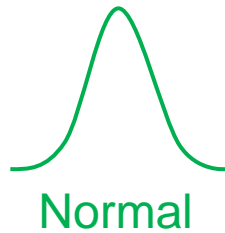


For emerging technologies, characterizing inputs' probability distribution functions (PDF) may be difficult

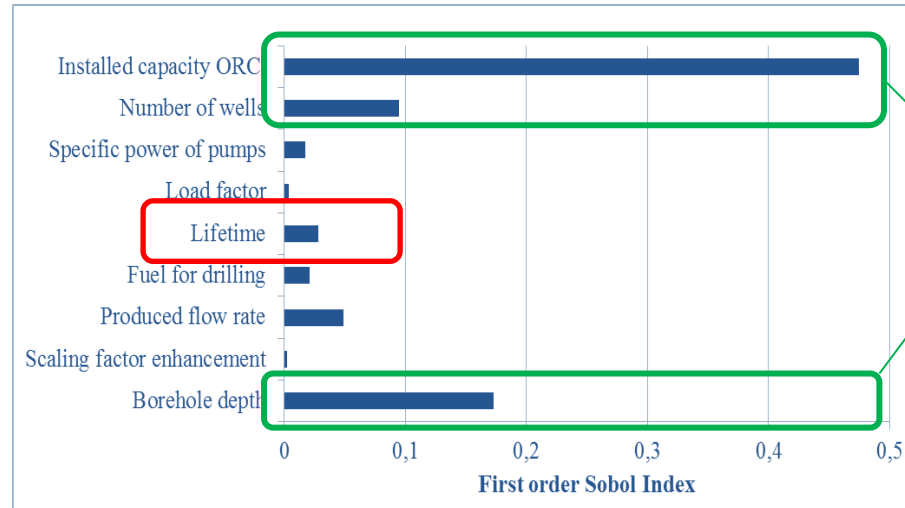


Which is the effect of changing PDF on inputs' ranking from GSA?

LIFETIME



Hypothesis (uncertain)



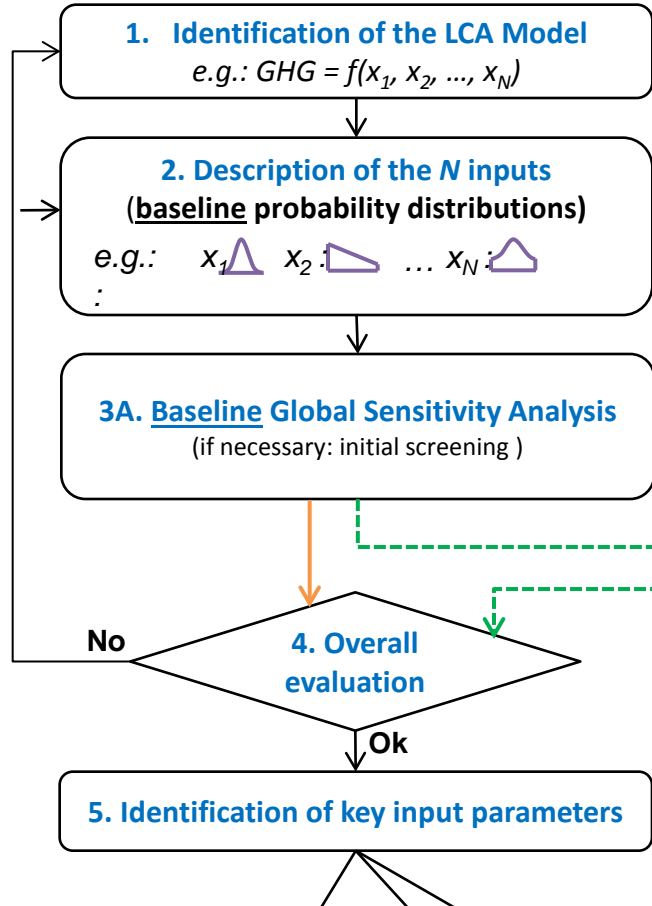
P_{ORC}, Nw, z :
Key parameters responsible for 75% of output variation



P_{ORC}, LT, z :
Key parameters

Proposed GSA approach for emerging technologies

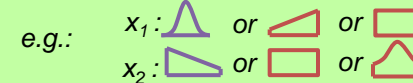
Baseline GSA approach



3B. Analysis of the influence of the inputs' description

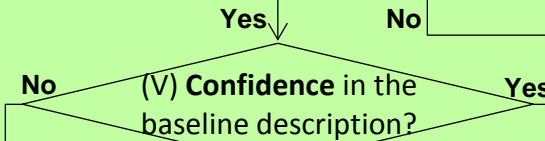
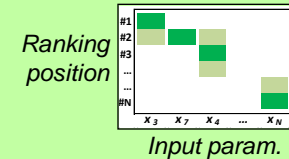
(I) Criteria to identify the set of key parameters

(II) Definition of **alternative** descriptions of the inputs:



(III) Reiteration of the Global Sensitivity Analysis

(IV) Influence of the inputs' description on the identification of the set of key parameters?



The baseline description of the inputs needs to be refined

No need to refine the baseline description of the inputs

Applications:

Simplified model

Other applications

(Cucurachi et al. 2016; Lacirignola et al. 2017)

Parameter	Value range [unit]	Baseline distribution (type1)	Alternative distributions			
			Type 2	Type 2	Type 4	Type 5
Borehole depth (z)	2,000 – 6,000 [Meters]	Uniform $\mu: 4,000 \quad \sigma: 1,155$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -11\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 11\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$
Scaling factor enhan. (Sfe)	0.5 – 10 [Ad.]	Trunc-lognormal $\mu: 2.10 \quad \sigma: 1.53$	 $\Delta\mu: 99\% \quad \Delta\sigma: 65\%$	 $\Delta\mu: 150\% \quad \Delta\sigma: 79\%$	 $\Delta\mu: 150\% \quad \Delta\sigma: 2\%$	 $\Delta\mu: 150\% \quad \Delta\sigma: 53\%$
Flow rate (f)	25 – 100 [kg/s]	Uniform $\mu: 62.5 \quad \sigma: 21.7$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -13\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 13\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$
Fuel for drilling (d)	3,000 – 7,000 [MJ/m]	Uniform $\mu: 5,000 \quad \sigma: 1,155$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -9\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 9\% \quad \Delta\sigma: -7\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$
Lifetime (LT)	20 – 40 [Years]	Trunc-gaussian $\mu: 30 \quad \sigma: 3.3$	 $\Delta\mu: 0\% \quad \Delta\sigma: 76\%$	 $\Delta\mu: -7\% \quad \Delta\sigma: 62\%$	 $\Delta\mu: 7\% \quad \Delta\sigma: 62\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: 51\%$
Load factor (LF)	0.85 – 0.95 [Ad.]	Uniform $\mu: 0.90 \quad \sigma: 0.03$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -1\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 1\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$
Pumps specific power (P_p)	3.6 – 8.6 [kW/(kg/s)]	Uniform $\mu: 6.1 \quad \sigma: 1.4$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -9\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 9\% \quad \Delta\sigma: -7\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$
Number of wells (Nw)	2 or 3 [Ad.]	50% 50% $\mu: 2.5 \quad \sigma: 0.5$	 $\Delta\mu: -8\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 8\% \quad \Delta\sigma: -8\%$	-	-
Installed capacity ORC (P_{ORC})	1,250 – 3,500 [kW]	Uniform $\mu: 2,375 \quad \sigma: 650$	 $\Delta\mu: 0\% \quad \Delta\sigma: -43\%$	 $\Delta\mu: -11\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 11\% \quad \Delta\sigma: -8\%$	 $\Delta\mu: 0\% \quad \Delta\sigma: -14\%$

Possible descriptions (probability distribution functions) for each of the 9 input parameters for EGS LCA model

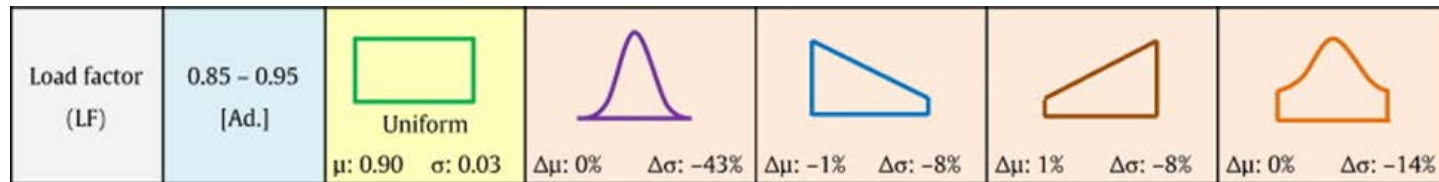
(Lacirignola et al. 2017)

Changing the distribution function for 1 input parameter and keeps other distributions as baseline

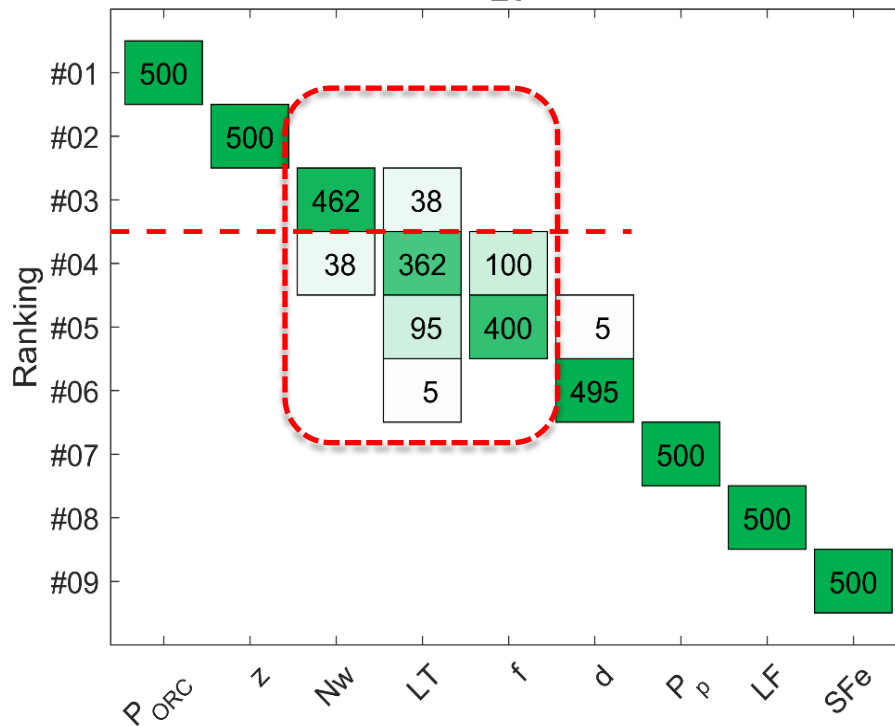
§ GSA	z	SFe	f	d	LF	LT	P _p	Nw	P _{ORC}
§1 (Baseline) ×100 bootstraps	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 2 (×100)	TYPE 2	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 3 (×100)	TYPE 3	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 4 (×100)	TYPE 4	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 5 (×100)	TYPE 5	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 6 (×100)	Baseline	TYPE 2	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 7 (×100)	Baseline	TYPE 3	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 8 (×100)	Baseline	TYPE 4	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
§ 9 (×100)	Baseline	TYPE 5	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline
[...]	[...]	[...]	[...]	[...]	[...]	[...]	[...]	[...]	[...]
§ 32 (×100)	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	TYPE 2
§ 33 (×100)	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	TYPE 3
§ 34 (×100)	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	TYPE 4
§ 35 (×100)	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	Baseline	TYPE 5

(Lacirignola et al. 2017)

For example, using the 5 possible distribution functions for **LIFETIME (LT)**:

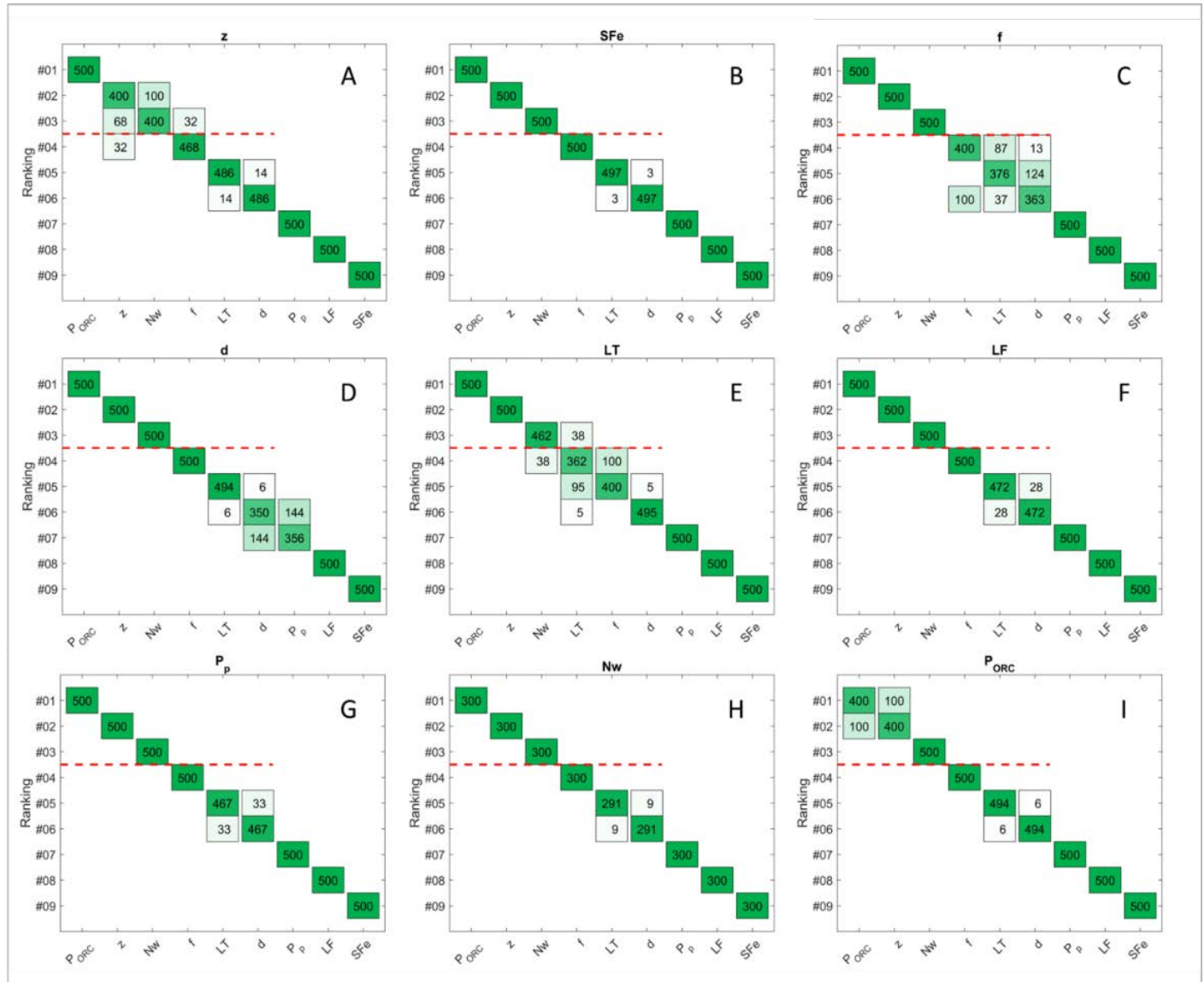


LT

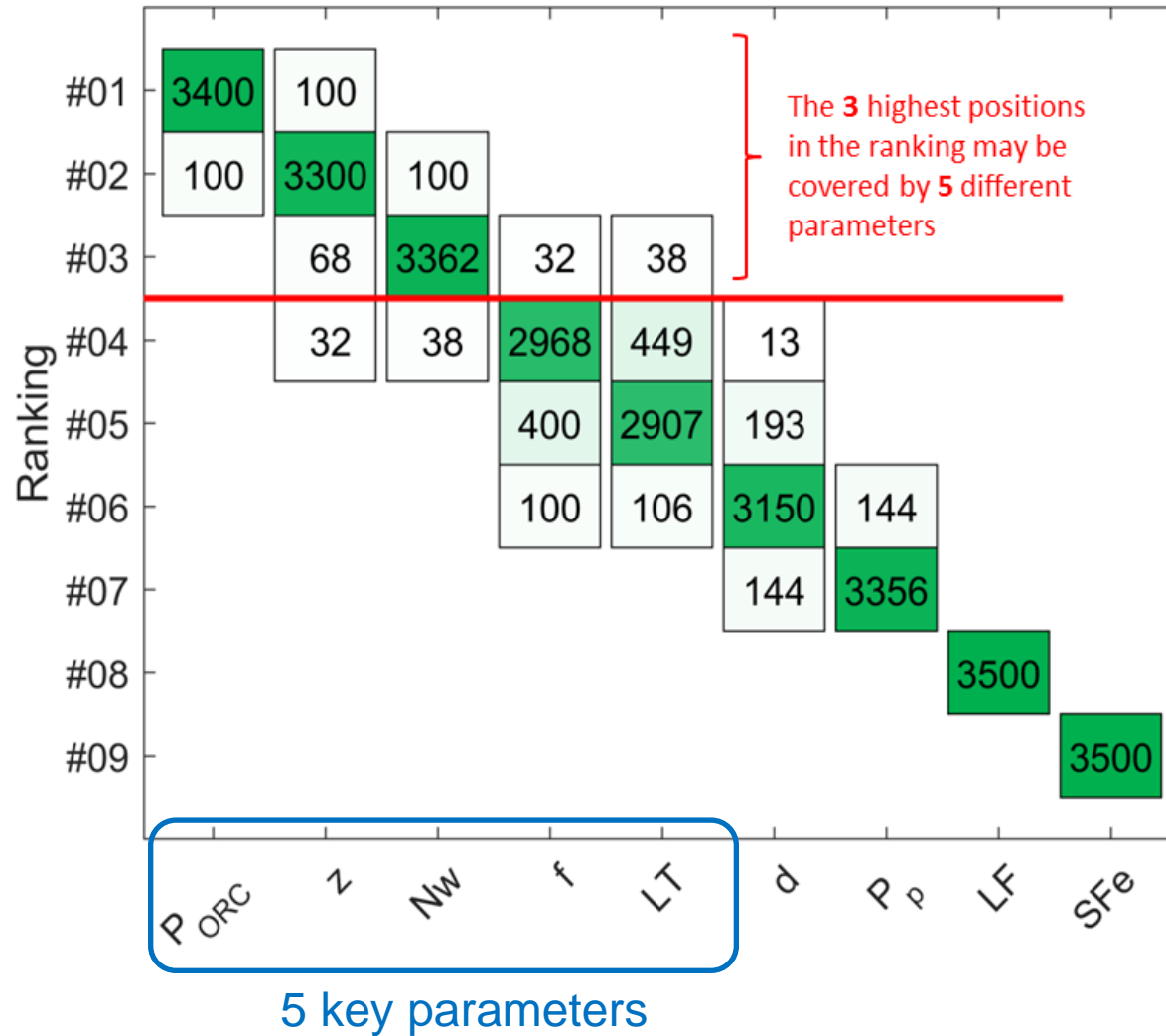


- Positions 1 and 2 always correspond to parameters P_{ORC} and z
- Positions 3, 4, 5 \Rightarrow influenced by LT distribution

For each of the 9 input parameters



Considering 3500 rankings after iterative GSA:



Identification of **5** key input parameters among the **9** initial ones
 → **Simplified model for LCA of EGS facilities**

5 key parameters

$$GHG_{EGS_Reduced} \left[\frac{gCO_2eq}{kWh} \right] = f(P_{ORC}, N_w, z, LT, f)$$

$$= \frac{N_w \cdot (\omega_1 \cdot z + \omega_2) + LT \cdot (\omega_3 \cdot f + \omega_4 \cdot P_{ORC})}{LT \cdot (P_{ORC} - f \cdot \omega_5)} \pm 5 \text{ gCO}_2\text{eq/kWh}$$

$$\omega_1 = 120.70 [gCO_2eq/(m \cdot h/y)]; \omega_2 = 5\,161.87 [gCO_2eq/(h/y)];$$

$$\omega_3 = 61.82 [gCO_2eq \cdot s/(kg \cdot h)]; \omega_4 = 6.42 [gCO_2eq/(kWh)]; \omega_5 = 6.10 [(kW \cdot s)/kg];$$

- From complete parametric model


$$GHG_{EGS} \left[\frac{g CO_2eq}{kWh} \right] = \frac{z \cdot Nw \cdot (\alpha_1 + \alpha_2 \cdot d) + LT \cdot f \cdot \alpha_3 + P_{ORC} \cdot LT \cdot \alpha_4 + Nw \cdot Sfe \cdot \alpha_5}{LF \cdot LT \cdot (P_{ORC} - f \cdot P_p) \cdot 8760}$$

- ... to simplified model

$$GHG_{EGS_Reduced} \left[\frac{gCO_2eq}{kWh} \right] = \frac{Nw \cdot (\omega_1 \cdot z + \omega_2) + LT \cdot (\omega_3 \cdot f + \omega_4 \cdot P_{ORC})}{LT \cdot (P_{ORC} - f \cdot \omega_5)}$$

ADVANTAGES

- ✓ Reduced number of input parameters (From 9 to 5)
- ✓ For some of the least influencing parameters, data were difficult to obtain → Simplified model facilitates data gathering

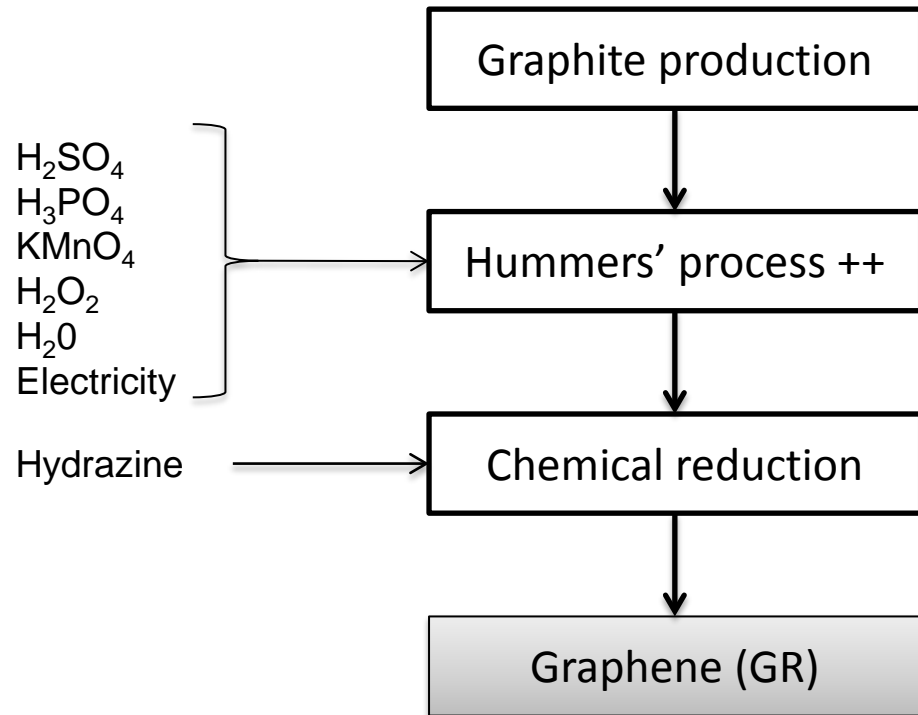
- Need for a specific approach to deal with large uncertainty of **emerging technologies** in LCA
- Global Sensitivity Analysis (GSA) based on variance-decomposition methods (e.g. Sobol) allows **key parameter identification** and ranking
- The protocol proposed for GSA of emerging technologies helped to evaluate the influence of **distribution functions** of input parameters in GSA results
-  **a simplified parametric equation** to estimate GHG impact from a reduced number of parameters was obtained.
- We aim to apply the same approach to deduce a set of simplified equations for a multi-criteria LCA

- Case study: Graphene (GR) production by **chemical reduction process**
(Based on publication by Arvidsson et al. 2014)

- No pilot/large-scale data
- Incomplete technology development
- Unknown future applications
- Data quality concerns



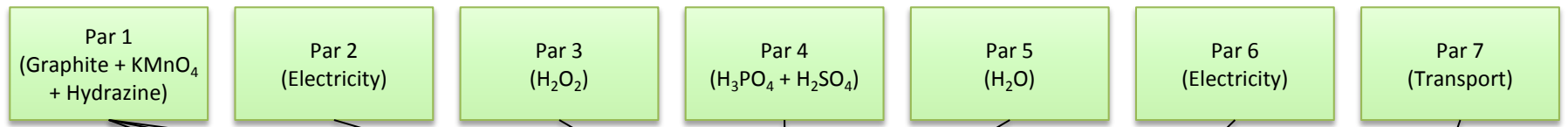
Emerging technology



Symbols	Parameters	Baseline scenario
Par 1	Graphite + Potassium permanganate (KMnO ₄) + Hydrazine	2.55 g / g of GR
Par 2	Electricity RER medium voltage - 1	8.5 MJ / g of GR
Par 3	Peroxide (H ₂ O ₂)	4.675 g / g of GR
Par 4	Phosphoric acid (H ₃ PO ₄) + Sulfuric acid (H ₂ SO ₄)	33.15 g / g of GR
Par 5	Deionised water	0.935 g / g of GR
Par 6	Electricity RER medium voltage - 2	0.15 MJ / g of GR
Par 7	Transport - lorry >32 tons class 5	0.259 kg·km / g of GR

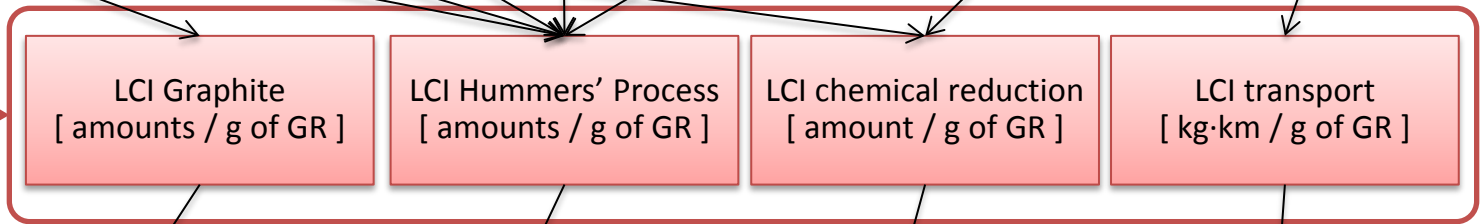
(Based on publication by Arvidsson et al. 2014)

7 independent input parameters



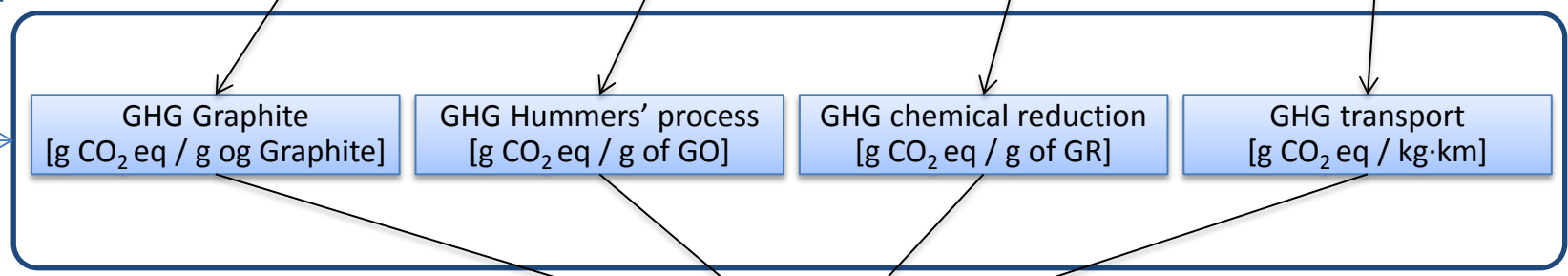
Life cycle inventory

Database
(e.g. Ecoinvent 3.3)

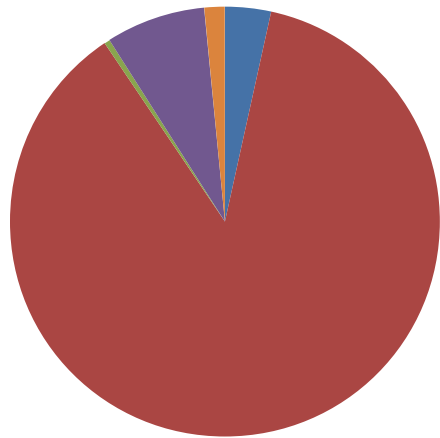


Life cycle impact assessment

Carbon footprints



Baseline result: 1.7 kg CO₂ eq./g of GR



- Graphite + Potassium permanganate (KMnO₄) + Hydrazine
- Electricity RER medium voltage - 1
- Peroxyde (H₂O₂)
- Phosphoric acid (H₃PO₄) + Sulfuric acid (H₂SO₄)
- Deionised water
- Electricity RER medium voltage - 2
- Transport - lorry >32 tons class 5

Carbon footprint contribution

1. Electricity for Hummers' process (Par 2)
2. Acids (Par 4)
3. Graphite + KMnO₄ + Hydrazine (Par 1)
4. Electricity for chemical reduction (Par 6)
5. Peroxide (Par 3)
6. Transport (Par 7)
7. Deionised water (Par 5)

Symbols	Parameters	Baseline scenario	GSD ² (Pedigree Matrix)
Par 1	Graphite + Potassium permanganate (KMnO ₄) + Hydrazine	2.55 g / g of GR	1.51
Par 2	Electricity RER medium voltage - 1	8.5 MJ / g of GR	1.51
Par 3	Peroxide (H ₂ O ₂)	4.675 g / g of GR	1.51
Par 4	Phosphoric acid (H ₃ PO ₄) + Sulfuric acid (H ₂ SO ₄)	33.15 g / g of GR	1.51
Par 5	Deionised water	0.935 g / g of GR	1.51
Par 6	Electricity RER medium voltage - 2	0.15 MJ / g of GR	1.50
Par 7	Transport - lorry >32 tons class 5	0.259 kg·km / g of GR	1.72

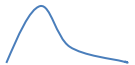


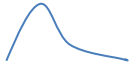
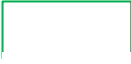

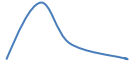














(Based on publication by Arvidsson et al. 2014)

Equivalent relative uncertainty

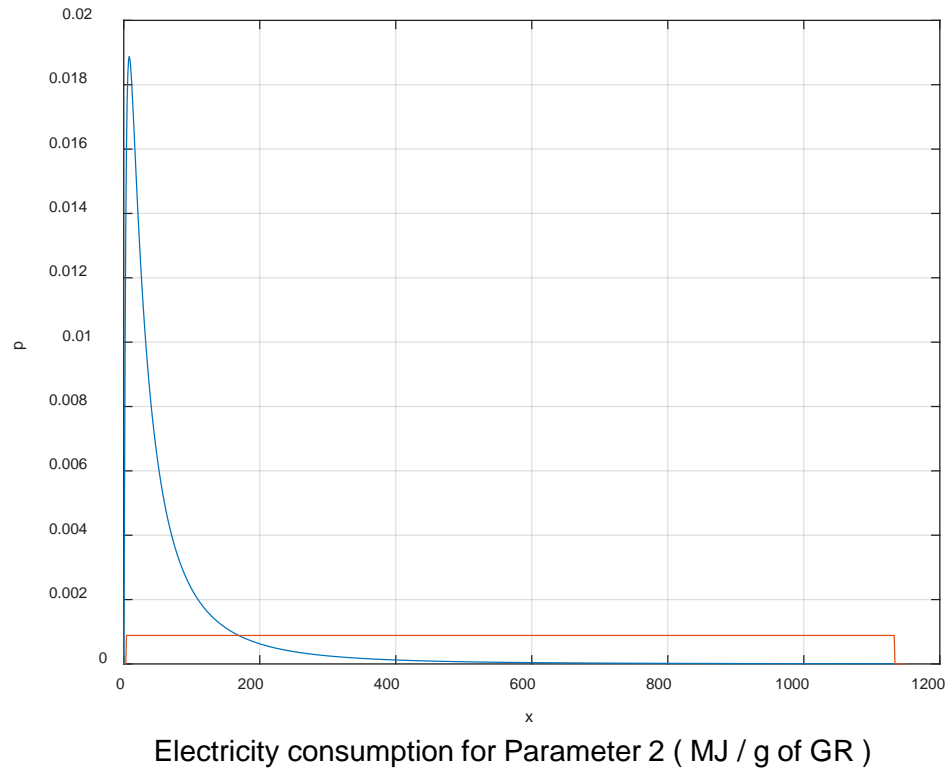
		Par 2	Par 6	Par 4	Par 1	Par 3	Par 7	Par 5
		Electricity - 1	Electricity - 2	Acids	Graphite + KMnO4 + Hydrazine	Peroxide	Transport	Water
Ranking	1	100 000						
	2			100 000				
	3				100 000			
	4		100 000					
	5					100 000		
	6						100 000	
	7							100 000

Symbols	Parameters	Baseline scenario	Value range
Par 1	Graphite + Potassium permanganate (KMnO ₄) + Hydrazine	2.55 g / g of GR	0.85 – 4.25 g
Par 2	Electricity RER medium voltage - 1	8.5 MJ / g of GR	3.4 – 1133 MJ
Par 3	Peroxide (H ₂ O ₂)	4.675 g / g of GR	0.85 – 8.5 g
Par 4	Phosphoric acid (H ₃ PO ₄) + Sulfuric acid (H ₂ SO ₄)	33.15 g / g of GR	22.1 – 44.2 g
Par 5	Deionised water	0.935 g / g of GR	25 – 100 kg
Par 6	Electricity RER medium voltage - 2	0.15 MJ / g of GR	0.06 – 6 MJ
Par 7	Transport - lorry >32 tons class 5	0.259 kg·km / g of GR	0.013 – 5.18 kg·km

(Based on publication by Arvidsson et al. 2014 and its references)

Parameters	Value range	Baseline distribution	Alternative distributions	
		Type 1	Type 2	Type 3
Par 1	0.85 – 4.25 g	 lognormal	 Uniform	 Triangular
Par 2	3.4 – 1133 MJ	 lognormal	 Uniform	 Triangular
Par 3	0.85 – 8.5 g	 lognormal	 Uniform	 Triangular
Par 4	22.1 – 44.2 g	 lognormal	 Uniform	 Triangular
Par 5	25 – 100 kg	 lognormal	 Uniform	 Triangular
Par 6	0.06 – 6 MJ	 lognormal	 Uniform	 Triangular
Par 7	0.013 – 5.18 kg·km	 lognormal	 Uniform	 Triangular

Difference between lognormal and uniform distribution for electricity used in Hummers' process



Pedigree approach propose much lower uncertainty than the value range found in the reference

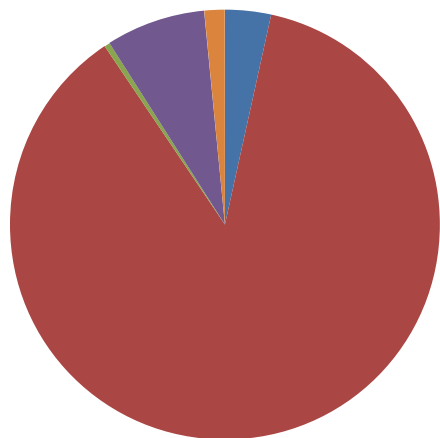
		Par 2	Par 6	Par 4	Par 1	Par 3	Par 7	Par 5
		Electricity - 1	Electricity - 2	Acids	Graphite + KMnO4 + Hydrazine	Peroxide	Transport	Water
Ranking	1	200 000						
	2		100 273	99 727				
	3			100 273	99 727			
	4		99 727		100 273			
	5					200 000		
	6						200 000	
	7							200 000

		Par 2	Par 6	Par 4	Par 1	Par 3	Par 7	Par 5
		Electricity - 1	Electricity - 2	Acids	Graphite + KMnO4 + Hydrazine	Peroxide	Transport	Water
Ranking	1	200 000						
	2		100 383	99 617				
	3			100 383	99 617			
	4		99 617		100 383			
	5					200 000		
	6						200 000	
	7							200 000

		Par 2	Par 6	Par 4	Par 1	Par 3	Par 7	Par 5
		Electricity - 1	Electricity - 2	Acids	Graphite + KMnO4 + Hydrazine	Peroxide	Transport	Water
Ranking	1	200 000						
	2		200 000					
	3			150 119	49 881			
	4			49 881	150 119			
	5					200 000		
	6						200 000	
	7							200 000

		Par 2	Par 6	Par 4	Par 1	Par 3	Par 7	Par 5
		Electricity - 1	Electricity - 2	Acids	Graphite + KMnO4 + Hydrazine	Peroxide	Transport	Water
Ranking	1	300 000						
	2		199 867	89 137	10 996			
	3			188 894	111 106			
	4		100 133	21 969	177 898			
	5					300 000		
	6						300 000	
	7							300 000

Baseline result: 1.7 kg CO₂ eq./g of GR



- Graphite + Potassium permanganate (KMnO₄) + Hydrazine
- Electricity RER medium voltage - 1
- Peroxyde (H₂O₂)
- Phosphoric acid (H₃PO₄) + Sulfuric acid (H₂SO₄)
- Deionised water
- Electricity RER medium voltage - 2
- Transport - lorry >32 tons class 5

Global sensitivity Analysis / Ranking

1. Electricity for Hummers' process (Par 2)
2. Acids (Par 4)
3. Graphite + KMnO₄ + Hydrazine (Par 1)
4. Electricity for chemical reduction (Par 6)
5. Peroxide (Par 3)
6. Transport (Par 7)
7. Deionised water (Par 5)

Thank you for your attention

Prospective LCA modelling

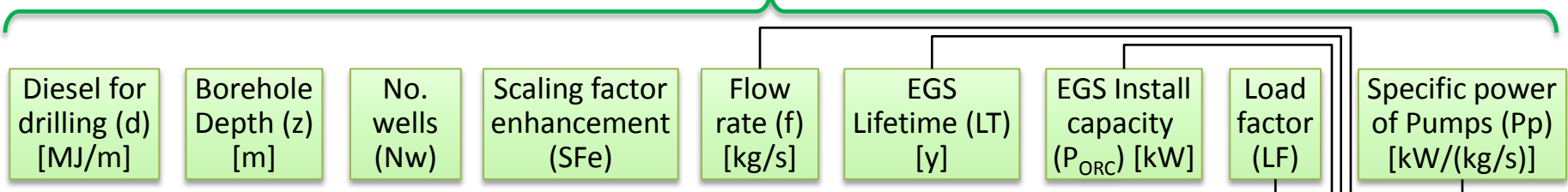
How to deal with uncertainties ?

Part I : A new approach based on GSA

Part II : The Graphene Case study

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Paula Pérez-López, Philippe Blanc, **Isabelle Blanc** (Centre O.I.E. - MINES ParisTech, FR)
Robin Girard (Centre PERSEE - MINES ParisTech, FR)
Didier Beloin-Saint-Pierre (EMPA, CH)

9 independent input parameters

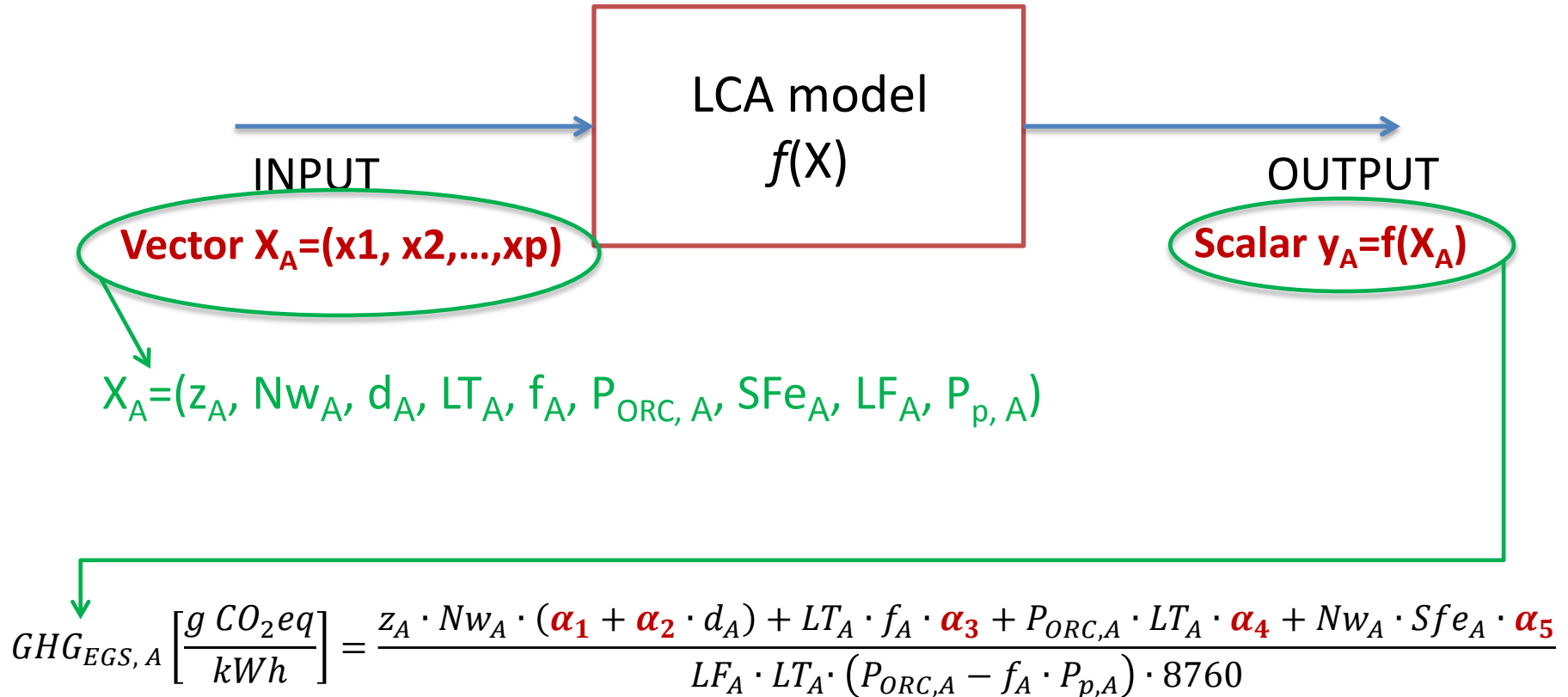


$$\text{Electricity production [kWh]} = LT \cdot LF \cdot (P_{ORC} - f \cdot P_p) \cdot 8760$$

Life-cycle electricity production [kWh]

Environmental impact [g CO₂eq/kWh] = **gCO₂eq** / kWh to electricity grid

A) General modeling framework for LCA



With $\alpha_1 = 498761.36 \text{ gCO}_2 \text{ eq/m}$; $\alpha_2 = 90.56 \text{ gCO}_2 \text{ eq/MJ}$; $\alpha_3 = 487363.03 \text{ gCO}_2 \text{ eq}\cdot\text{s}/(\text{kg}\cdot\text{y})$;
 $\alpha_4 = 50603.13 \text{ gCO}_2 \text{ eq}/(\text{kW}\cdot\text{y})$; $\alpha_5 = 25757089.05 \text{ gCO}_2 \text{ eq}$